

Relay Systems - The Simplest Hybrid Systems?

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1. Introduction
2. Examples of Relay Systems
3. Relay Auto-Tuning
4. Limit Cycles
5. Summary

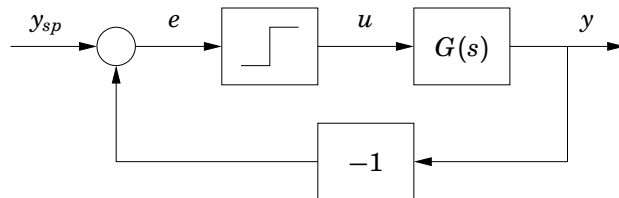
Thanks to K. H. Johansson, A Rantzer and S. E. Mattson

Introduction

- The Simplest hybrid system?
 - Two discrete states
 - Linear continuous behavior
- Relay systems are common
- Relay systems have been studied for a long time
- Relays systems are still widely used
 - Delta-Sigma modulators
 - Relay auto-tuning
- Relay systems have rich behavior
- Challenges
- Can theory for hybrid systems help?

A Challenge

Understand the behavior of the system



Some things are well known but important problems remain
Find all transfer functions such that there is a stable limit cycle

I hope to tell you why this is interesting

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Relay Systems are Common

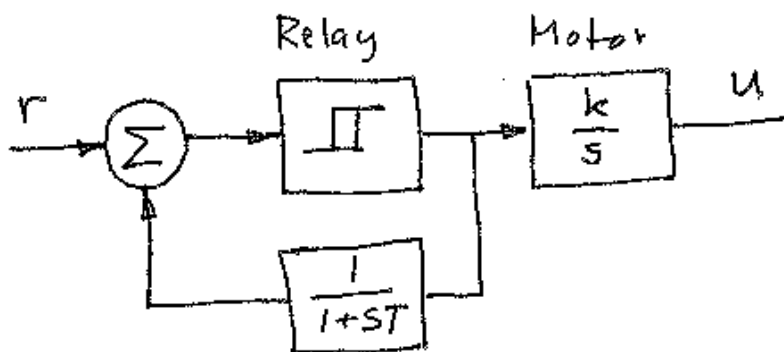
Applications of relay feedback include

- On-off control, temperature control (Hawkins,1887)
- Amplifiers
- Self-oscillating adaptive systems
- Relay auto-tuning
- DC/DC converters
- Δ - Σ modulators
- Coulomb friction
- Variable structure systems

A Classic Field

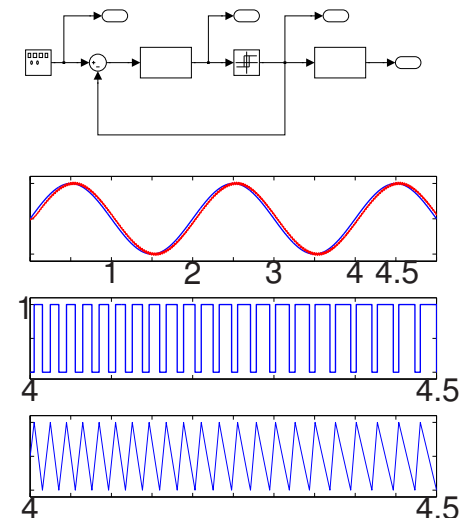
- J. T. Hawkins Automatic regulators for heating apparatus. Trans ASME 1887.
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- Ahterton Nonlinear Control Engineering. 1975
- Tsytkin Relay Control Systems. 1984
- Filippov Differential equations with Discontinuous Right Hand Side. 1988.
- Utkin. Sliding Mode Control. 1992
- Aizerman 1974

PI Temperature Controller



$$G(s) = \frac{k}{s} \frac{k_r}{1 + \frac{k_r}{1+sT}} = k \frac{1+sT}{s} = kT + \frac{k}{s}$$

The Delta-Sigma Modulator



Cousins of the Delta-Sigma Modulator

- One-bit AD converter
 - Sampled versions
 - Telecom systems
- One bit stereo amplifier

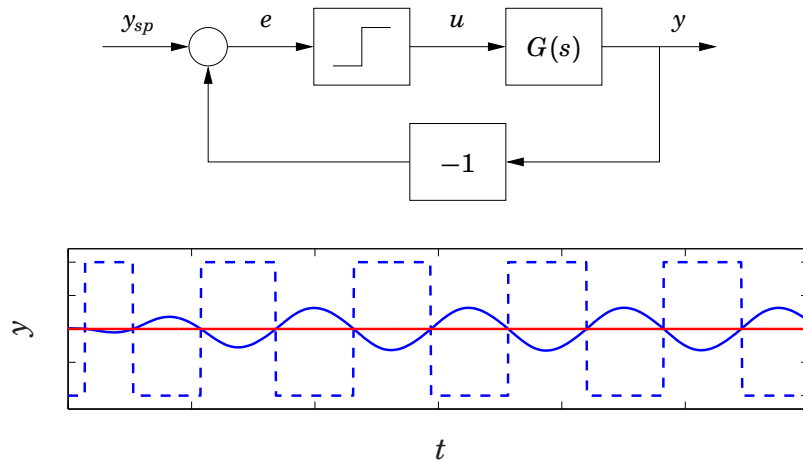
Challenging problems

- How to avoid ringing
- System design
 - Trial and error - patent coefficients
 - Model predictive control
 - Daniel Quevedo: Quantized Moving Horizon Optimization PhD thesis University of Newcastle

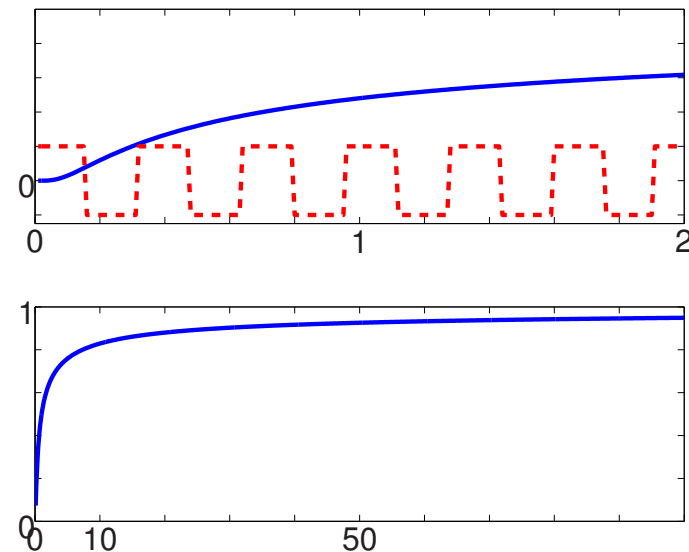
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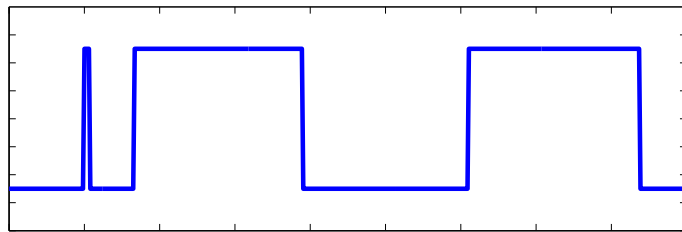
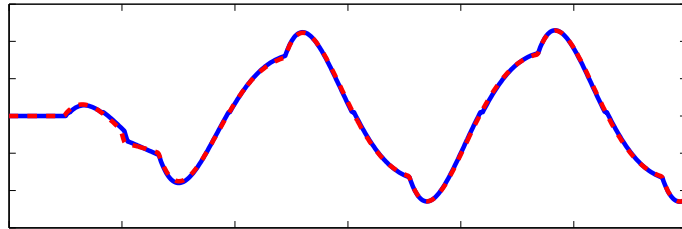
Relay Auto-Tuning



Short Experiment Time $G(s) = \exp(-\sqrt{s})$

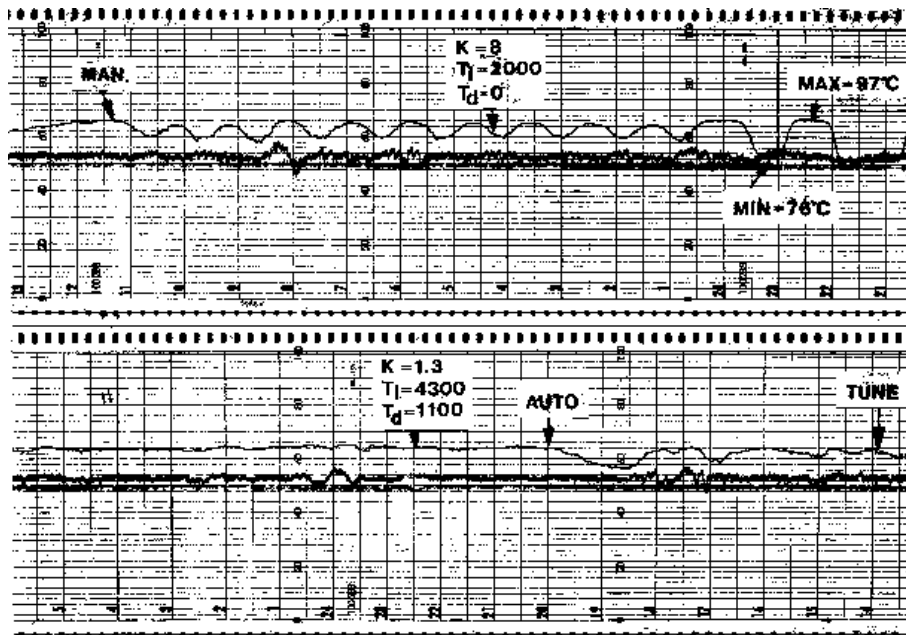


Good Excitation



Commercial Auto-Tuners

- Easy to use
 - one-button tuning
- Robust
- Many versions
 - Stand alone
 - DCS systems
 - Estimation methods
 - Control design
- Large numbers
- Good industrial experience

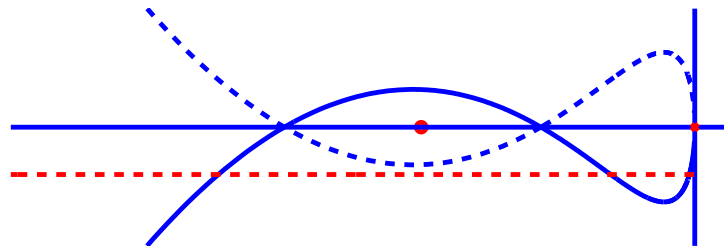


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Limit Cycles

- Describing functions



- Tsytkins frequency domain conditions
- Necessary conditions
- Local stability
- Limit cycles with chattering

Necessary Conditions

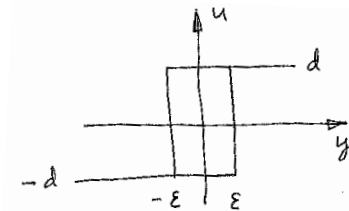
Assume $CB = 0$, relay with hysteresis. Assume that the system is in state $-a$ on a symmetrical periodic orbit when control switches from $-d$ to d . Integrate over a half period h

$$\frac{dx}{dt} = Ax + Bu, \quad y = Cx$$

$$x(h) = a = -e^{Ah}a + \int_0^h e^{As} ds Bd$$

$$= -\Phi(h)a + \Gamma(h)d$$

$$Cx(h) = \varepsilon$$



$$f(h) = C(I + e^{Ah})^{-1} \int_0^h e^{As\tau} d\tau = \frac{\varepsilon}{d}$$

Necessary Conditions for a Limit Cycle

Consider a linear system with hysteretic relay feedback. Assume that there exists a symmetric periodic solution with period $T = 2h$. Then the following conditions hold.

$$(i) \quad f(h) = C(I + e^{Ah})^{-1} \int_0^h e^{A\tau} B d\tau = \frac{\varepsilon}{d}$$

$$(ii) \quad y(t) = C \left(e^{At}a - \int_0^t e^{A\tau} d\tau Bd \right) < \varepsilon \text{ for } 0 \leq t < h$$

It follows from (ii) that

$$y'(0) = -Ca$$

The periodic solution is obtained with the initial condition

$$x(0) = a = (I + e^{Ah})^{-1} \int_0^h e^{A\tau} B d\tau d$$

Local Stability

Assume that there is a symmetric periodic solution with period $2h$. Let a be the initial state that generates the periodic motion. The Jacobian of the Poincaré map is given by

$$W = \left(I - \frac{vC}{Cv} \right) e^{Ah},$$

where $v = Aa + Bd$. The limit cycle is locally stable if and only if W has all its eigenvalues inside the unit disk.

The eigenvalues give the convergence rate.

Global stability. Conditions given by Goncalves using Lyapunov functions and LMIs.

Analysis of Limit Cycles for a Particular System

Straight forward computations

- Solve

$$f(h) = C(I + e^{Ah})^{-1} \int_0^h e^{A\tau} B d\tau = \frac{\varepsilon}{d}$$

- Compute initial state

$$a = (I + e^{Ah})^{-1} \int_0^h e^{A\tau} B d\tau d$$

- Check y
- Check global stability using LMIs

Frequency Domain Interpretation

Let $H(z)$ be the pulse transfer function corresponding to zero-order hold sampling of the system with sampling period h

$$\frac{dx}{dt} = Ax + Bu, \quad y = Cx$$

i.e.

$$H(z) = C(zI - \Phi(h))^{-1} \Gamma(h)$$

The the condition

$$f(h) = C(I + \Phi(h))^{-1} \Gamma(h) = \frac{\varepsilon}{d}$$

can be written as

$$H(-1) = -\frac{\varepsilon}{d}$$

Physical interpretation! Infinite dimensional systems.

Frequency Domain Interpretation - Tsytkin Locus

Condition for oscillation

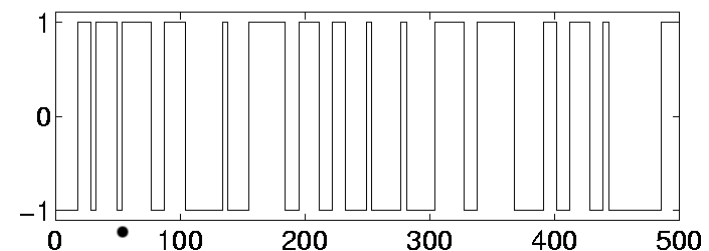
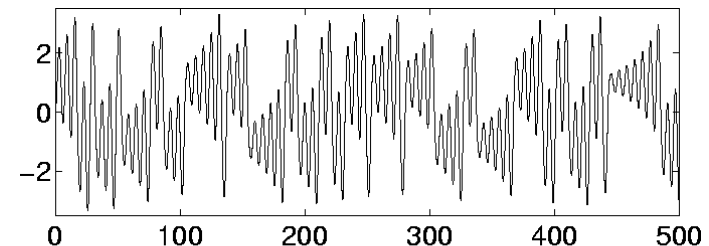
$$H(z) = \sum_{n=-\infty}^{\infty} \frac{1 - z^{-1}}{\log z + 2\pi in} G\left(\frac{1}{h} \log z + \frac{2\pi in}{h}\right) = -\frac{\varepsilon}{d}$$

Introducing $\omega = \pi/h$ gives

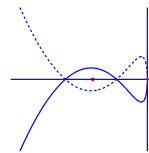
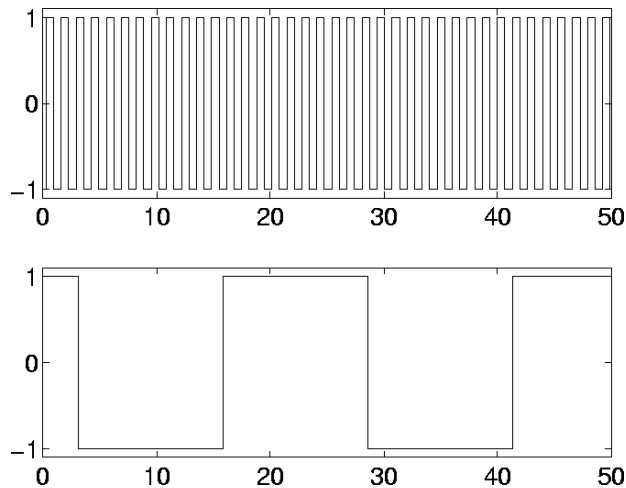
$$H(-1) = \frac{2}{i\pi} \sum_{n=-\infty}^{\infty} \frac{G(i\omega(1 + 2n))}{1 + 2n} \approx \frac{4}{i\pi} \text{Im } G(i\omega)$$

and the condition for oscillation is that the Nyquist plot of $G(s)$ intersects the half line $s = -i\varepsilon\pi/4d$. (Describing function condition.) The Tsytkin locus (hodograph) gives exact condition.

Asymmetrical Oscillations $G(s) = \frac{1}{s^2 - 0.1s + 1}$



Many Limit Cycles $\frac{(s+1)^2}{(s+0.1)^3(s+7)^2}$



Limit Cycles with Sliding Modes $\frac{(s-1)^2}{(s+1)^3}$

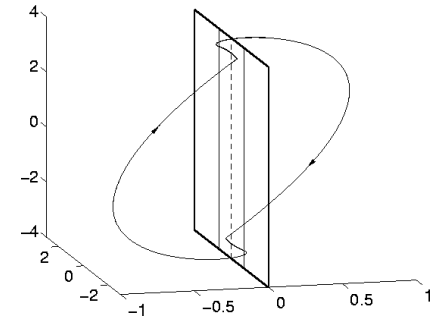
$$\dot{x}(t) = \begin{pmatrix} -3 & 1 & 0 \\ -3 & 0 & 1 \\ -1 & 0 & 0 \end{pmatrix} x(t) + \begin{pmatrix} 1 \\ -2 \\ 1 \end{pmatrix} u(t)$$

$$y(t) = \begin{pmatrix} 1 & 0 & 0 \end{pmatrix} x(t)$$

$$u(t) = -\text{sgn } y(t) = -\text{sgn}(x_1 + u)$$

Sliding mode $|x_1| < 1$

$$\begin{aligned} x_1 &= 0 \\ \frac{dx_2}{dt} &= x_3 \\ \frac{dx_3}{dt} &= 0 \end{aligned}$$



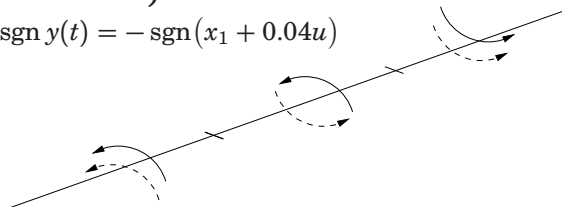
Limit Cycles with Sliding Modes $G(s) = \frac{(s-0.2)^2}{(s+1)^4}$

$$\dot{x}(t) = \begin{pmatrix} -4 & 1 & 0 & 0 \\ -6 & 0 & 1 & 0 \\ -4 & 0 & 0 & 1 \\ -1 & 0 & 0 & 0 \end{pmatrix} x(t) + \begin{pmatrix} 0 \\ 1 \\ -0.4 \\ 0.04 \end{pmatrix} u(t)$$

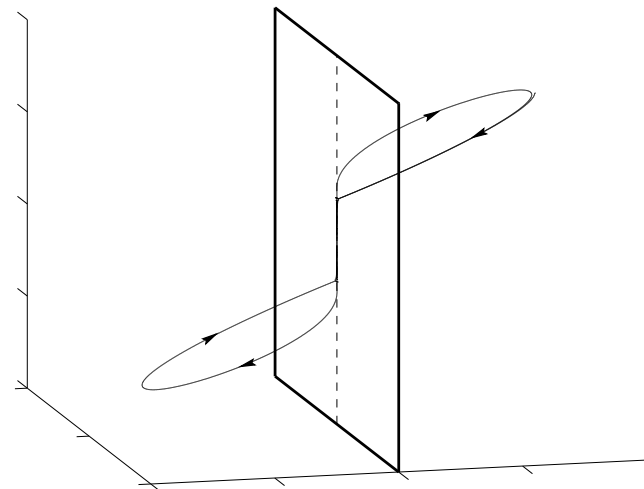
$$y(t) = \begin{pmatrix} 1 & 0 & 0 & 0 \end{pmatrix} x(t)$$

$$u(t) = -\text{sgn } y(t) = -\text{sgn}(x_1 + 0.04u)$$

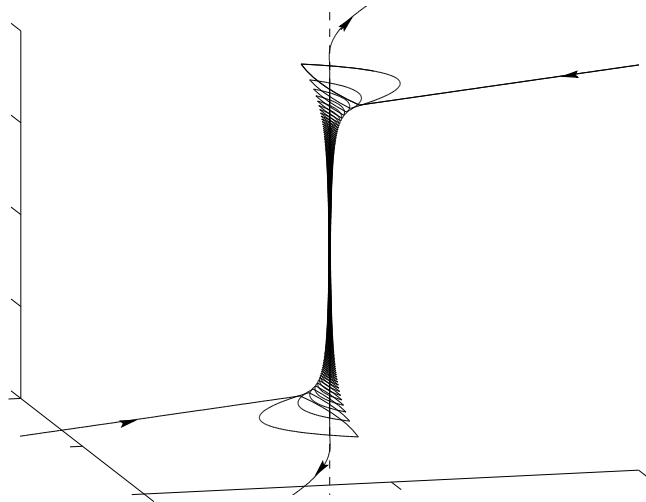
$CB = 0, CAB = 1$
2nd order sliding
 $|x_1| < 0.04$



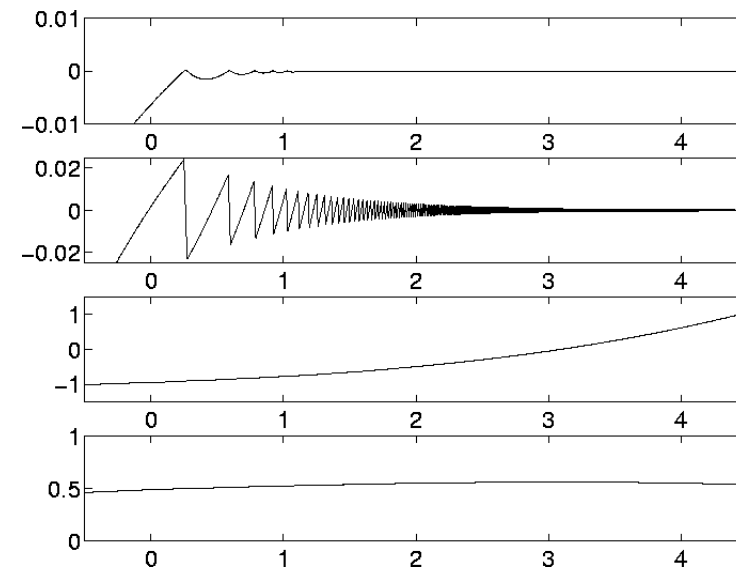
Projection of State Space on R^3



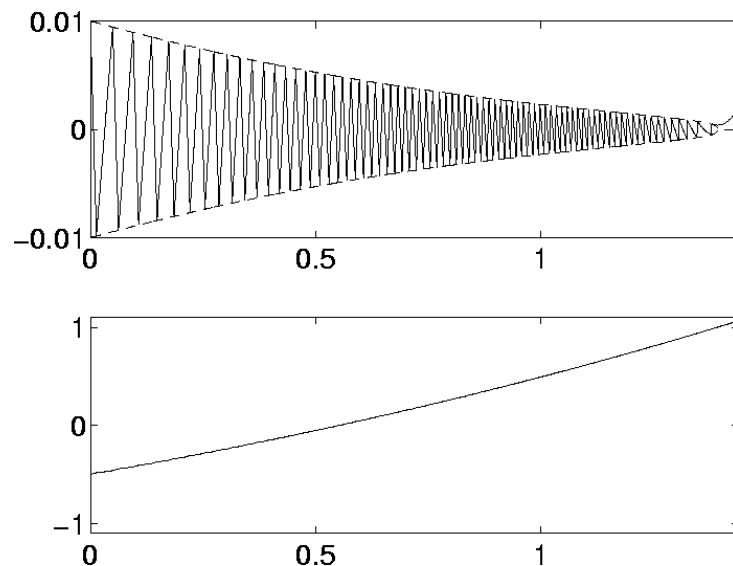
Projection of State Space on R^3 - Details



Time Functions



Accurate Estimates of Amplitudes



Simulation Difficult when Chattering Occurs

- Hybrid systems very useful
 - Detect that chattering occurs
 - Switch to Fillipov solution
 - Switch to regular solver when chattering stops $x_1 = 1$!
- Detection straight forward analytically but difficult to do automatically
- Omola-Omsim (Mattson et al)
- Modelica <http://modelica.org>

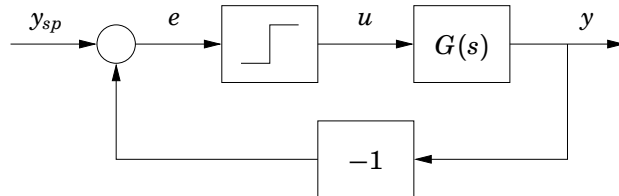
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Summary

- Relay system
 - Simple discrete behavior - only two states
 - Continuous behavior - linear
- In spite of this they have rich behavior
- Many useful applications
 - Simple feedback loops
 - Delta-sigma modulators
 - Relay auto tuners
- Challenging problems
 - Sampling theorems for amplitude quantized signals
 - Design theory for delta-sigma modulators
 - Classify systems where relay tuning works

Classify Systems where Relay Feedback Works



Find all transfer functions such that there is a stable limit cycle!

Conjectures

- Monotone frequency responses
- Almost monotone step responses

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